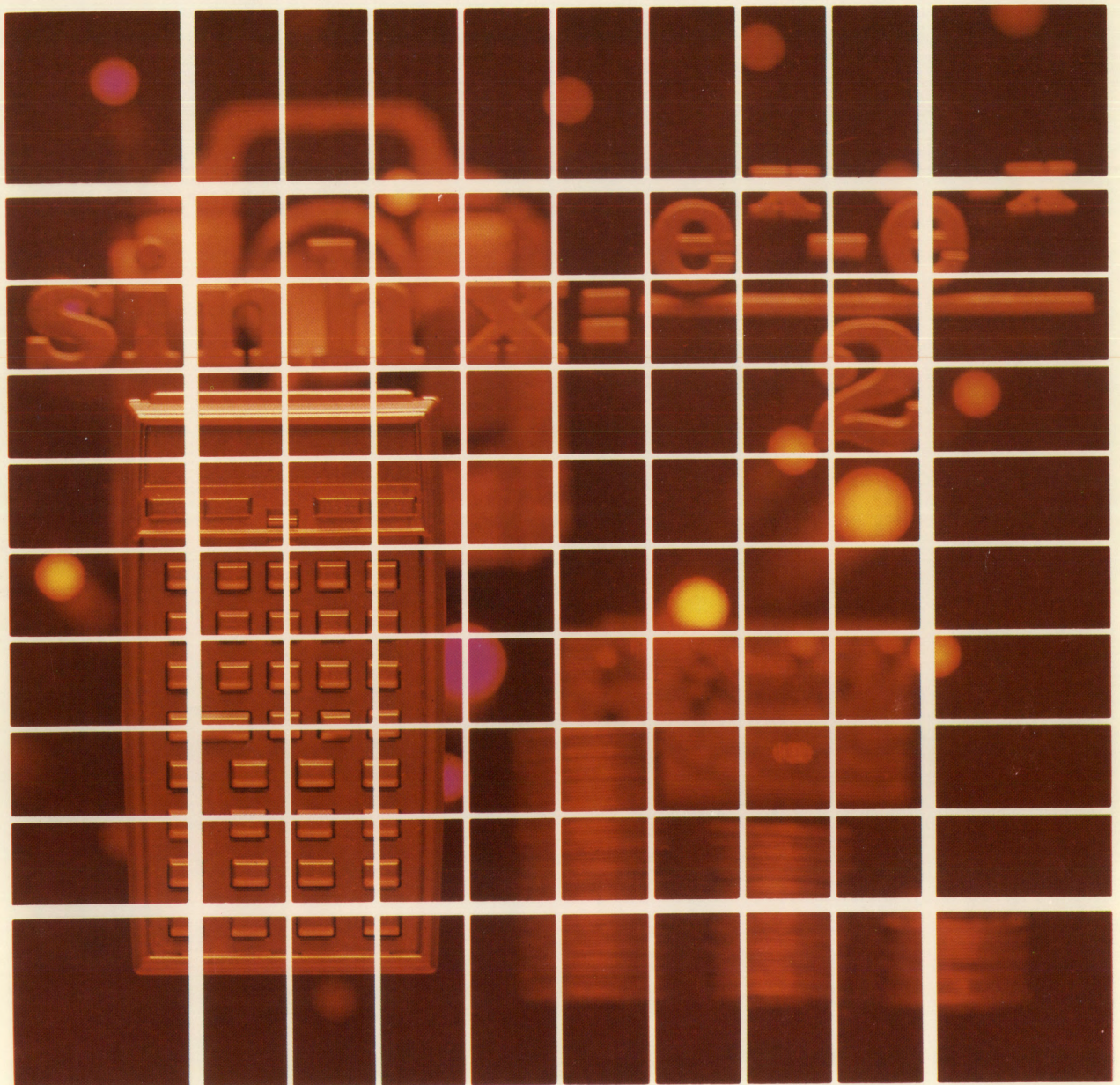


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HP-41C

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# Fluid Dynamics and Hydraulics



## **NOTICE**

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## INTRODUCTION

This HP-41C Solutions book was written to help you get the most from your calculator. The programs were chosen to provide useful calculations for many of the common problems encountered.

They will provide you with immediate capabilities in your everyday calculations and you will find them useful as guides to programming techniques for writing your own customized software. The comments on each program listing describe the approach used to reach the solution and help you follow the programmer's logic as you become and expert on your HP calculator.

### KEYING A PROGRAM INTO THE HP-41C

There are several things that you should keep in mind while you are keying in programs from the program listings provided in this book. The output from the HP 82143A printer provides a convenient way of listing and an easily understood method of keying in programs without showing every keystroke. This type of output is what appears in this handbook. Once you understand the procedure for keying programs in from the printed listings, you will find this method simple and fast. Here is the procedure:

1. At the end of each program listing is a listing of status information required to properly execute that program. Included is the SIZE allocation required. Before you begin keying in the program, press **XEQ** **ALPHA** SIZE **ALPHA** and specify the allocation (three digits; e.g., 10 should be specified as 010).

Also included in the status information is the display format and status of flags important to the program. To ensure proper execution, check to see that the display status of the HP-41C is set as specified and check to see that all applicable flags are set or clear as specified.

2. Set the HP-41C to PRGM mode (press the **PRGM** key) and press **GT0** **0** **0** to prepare the calculator for the new program.
3. Begin keying in the program. Following is a list of hints that will help you when you key in your programs from the program listings in this handbook.
  - a. When you see " (quote marks) around a character or group of characters in the program listing, those characters are ALPHA. To key them in, simply press **ALPHA**, key in the characters, then press **ALPHA** again. So "SAMPLE" would be keyed in as **ALPHA**"SAMPLE"**ALPHA**.
  - b. The diamond in front of each LBL instruction is only a visual aid to help you locate labels in the program listings. When you key in a program, ignore the diamond.
  - c. The printer indication of divide sign is /. When you see / in the program listing, press **+**.
  - d. The printer indication of the multiply sign is  $\times$ . When you see  $\times$  in the program listing, press **x**.
  - e. The † character in the program listing is an indication of the **APPEND** function. When you see †, press **APPEND** in ALPHA mode (press **ALPHA** and the K key).
  - f. All operations requiring register addresses accept those addresses in these forms:

nn (a two-digit number)

IND nn (INDIRECT: **IND**, followed by a two-digit number)

X, Y, Z, T, or L (a STACK address: **STO** followed by X, Y, Z, T, or L)

IND X, Y, Z, T or L (INDIRECT stack: **IND** followed by X, Y, Z, T, or L)

Indirect addresses are specified by pressing **IND** and then the indirect address. Stack addresses are specified by pressing **STO** followed by X, Y, Z, T, or L. Indirect stack addresses are specified by pressing **IND** and X, Y, Z, T, or L.

#### Printer Listing

```

01♦LBL "SAM
PLE"
02 "THIS IS
A "
03 "†SAMPLE
"
04 AVIEW
05 6
06 ENTER†
07 -2
08 /
09 ABS
10 STO IND
L
11 "R3="
12 ARCL 03
13 AVIEW
14 RTN
    
```

#### Keystrokes

```

LBL ALPHA SAMPLE ALPHA
ALPHA THIS IS A ALPHA
ALPHA APPEND SAMPLE
AVIEW ALPHA
6
ENTER†
2 CHS
+
XEQ ALPHA ABS ALPHA
STO 0 L
ALPHA R3= ARCL 03
AVIEW
ALPHA
RTN
    
```

#### Display

```

01 LBLT SAMPLE
02T THIS IS A
03T † SAMPLE
04 AVIEW
05 6
06 ENTER↑
07 -2
08 /
09 ABS
10 STO IND L
11T R3=
12 ARCL 03
13 AVIEW
14 RTN
    
```

## FLUID DYNAMICS AND HYDRAULICS

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	Solves flow problems using Manning flow formulae.	
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	Given surface coefficient (n) and any three of the following: 1) Flow 2) Slope 3) Pipe diameter 4) Depth %, the fourth is computed. Also computes velocity.	
4.	FORCES AT BENDS AND FITTINGS.....	20
	Solves for force due to a change in velocity of a fluid at a bend or fitting.	
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	Solves Valve Coefficient (Cv) for valves used in Liquid, Gas, Vapor and Steam.	
*6.	PIPE NETWORK ANALYSIS.....	31
	Solves equivalent length of a pipe using the Hazen-Williams equation. This allows for analysis of a water distribution system using the Hardy-Cross method.	
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	Solves for orifice bore and differential pressure across an orifice with flange taps for gas flow.	
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9.	COMPRESSIBLE FLOW IN VARIABLE AREA DUCTS.....	53
	Solves the area ratio mach number relationship for isentropic flow of a perfect gas in a variable area duct.	
10.	FLOOD ROUTING AND HYDROGRAPHS.....	59
	Solves for a unit hydrograph or a soil conservation service hydrograph given peak time and flow.	

\* Requires at least one additional memory module.

## CONDUIT FLOW

This program solves for the average velocity, or the pressure drop for viscous, incompressible flow in conduits.

Equations:

$$v^2 = \frac{\Delta P / \rho}{2 \left( f \frac{L}{D} + \frac{K_T}{4} \right)}$$

For laminar flow ( $Re < 2300$ )

$$f = 16/Re.$$

For turbulent flow ( $Re > 2300$ )

$$\frac{1}{\sqrt{f}} = 1.737 \ln \frac{D}{\epsilon} + 2.28 - 1.737 \ln \left( 4.67 \frac{D}{\epsilon Re \sqrt{f}} + 1 \right)$$

is solved by Newton's method.

$$\frac{1}{\sqrt{f_0}} = 1.737 \ln \frac{D}{\epsilon} + 2.28$$

is used as an initial guess in the iteration.

where:  $Re$  is the Reynolds number, defined as  $\rho Dv/\mu$ ;

$D$  is the pipe diameter;

$\epsilon$  is the dimension of irregularities in the conduit surface (see table 2);

$f$  is the Fanning friction factor for conduit flow;

$\Delta P$  is the pressure drop along the conduit;

$\rho$  is the density of the fluid;

$\mu$  is the viscosity of the fluid;

$\nu$  is the kinematic viscosity of the fluid and  $\mu = \rho\nu$ ;

$L$  is the conduit length;

$v$  is the average fluid velocity;

$K_T$  is the total of the applicable fitting coefficients in table 1.

Table 1  
Fitting Coefficients

Fitting	K
Globe valve, wide open	7.5—10
Angle valve, wide open	3.8
Gate valve, wide open	0.15—0.19
Gate valve, 3/4 open	0.85
Gate valve, 1/2 open	4.4
Gate valve, 1/4 open	20
90° elbow	0.4—0.9
Standard 45° elbow	0.35—0.42
Tee, through side outlet	1.5
Tee, straight through	.4
180° bend	1.6
Entrance to circular pipe	0.25—0.50
Sudden expansion	$(1 - A_{up}/A_{dn})^{2*}$
Acceleration from $v=0$ to $v=v_{entrance}$	1.0

\* $A_{up}$  is the upstream area and  $A_{dn}$  is the downstream area.

Table 2  
Surface Irregularities

Material	$\epsilon$ (feet)	$\epsilon$ (meters)
Drawn or Smooth Tubing	$5.0 \times 10^{-6}$	$1.5 \times 10^{-6}$
Commercial Steel or Wrought Iron	$1.5 \times 10^{-4}$	$4.6 \times 10^{-5}$
Asphalted Cast Iron	$4.0 \times 10^{-4}$	$1.2 \times 10^{-4}$
Galvanized Iron	$5.0 \times 10^{-4}$	$1.5 \times 10^{-4}$
Cast Iron	$8.3 \times 10^{-4}$	$2.5 \times 10^{-4}$
Wood Stave	$6.0 \times 10^{-4}$ to	$1.8 \times 10^{-4}$ to
	$3.0 \times 10^{-3}$	$9.1 \times 10^{-4}$
Concrete	$1.0 \times 10^{-3}$ to	$3.0 \times 10^{-4}$ to
	$1.0 \times 10^{-2}$	$3.0 \times 10^{-3}$
Riveted Steel	$3.0 \times 10^{-3}$ to	$9.1 \times 10^{-4}$ to
	$3.0 \times 10^{-2}$	$9.1 \times 10^{-3}$

Reference:

Welty, Wicks, Wilson, *Fundamentals of Momentum, Heat and Mass Transfer*, John Wiley and Sons, Inc., 1969.

## Remarks:

The correlation gives meaningless results in the region  $2300 < Re < 4000$ .

The solution requires an iterative procedure. The time for solution will range from 10 seconds for  $\Delta P$ , to several minutes for  $v$ . The display setting is used to determine when the solution for  $v$  is adequately accurate. Time for solution of  $v$  is roughly proportional to the number or significant digits in the display setting.

If the conduit is not circular, an equivalent diameter may be calculated using the formula below:

$$D_{eq} = 4 \frac{\text{cross sectional area}}{\text{wetted perimeter}}$$

Unitary consistency must be maintained.

## Example:

A heat exchanger has 20, 3 meter tube passes (60 m of pipe) with 180 degrees bends connecting each pair of tubes (from table 1,  $K_T = 10 \times 1.6$ ). The fluid is water ( $\nu = 9.3 \times 10^{-7} \text{ m}^2/\text{s}$ ,  $\rho = 10^3 \text{ kg/m}^3$ ). The surface roughness is  $3 \times 10^{-4} \text{ m}$  and the diameter is  $2.54 \times 10^{-2} \text{ m}$ . If the fluid velocity is 3.05 m/s, what is the pressure loss? What is the Reynolds number? What is the Fanning friction factor?

## Keystrokes:

[XEQ] [ALPHA] SIZE [ALPHA] 015  
 [////] [ENG] 3  
 [XEQ] [ALPHA] CONDUIT [ALPHA]  
 9.3 [EEX] [CHS] 7 [ENTER↑]  
 [EEX] 3 [X] [R/S]  
 [EEX] 3 [R/S]  
 3 [EEX] [CHS] 4 [R/S]  
 60 [R/S]  
 2.54 [EEX] [CHS] 2 [R/S]  
 16 [R/S]  
 3.05 [R/S]  
 [R/S]  
 [R/S]  
 [R/S]

## Display:

U=?  
 RHO=?  
 E=?  
 L=?  
 D=?  
 KT=?  
 V=?  
 DP=?  
 DP=521.9E3  
 Re=83.30E3  
 F=10.18E-3





# Program Listings

01*LBL "CON DUIT"		51 X<>Y	
02 "U=?"		52 X≠Y?	
03 PROMPT		53 GTO 03	
04 STO 09		54 "V="	
05 "RHO=?"	Input	55 RCL 02	
06 PROMPT		56 GTO 10	
07 STO 10		57*LBL 09	
08 ST/ 09		58 RCL 10	
09 "E=?"		59 RCL 13	
10 PROMPT		60 RCL 14	
11 STO 14		61 /	
12 "L=?"		62 STO 06	
13 PROMPT		63 LN	
14 STO 03		64 1.737	
15 "D=?"		65 STO 07	
16 PROMPT		66 *	
17 STO 13		67 2.28	
18 "KT=?"		68 +	
19 PROMPT		69 STO 12	
20 4		70 STO 05	
21 /		71 FS? 00	
22 STO 08		72 GTO 07	
23*LBL "CHA NGE"		73*LBL 08	
24 CF 22		74 16	
25 "V=?"		75 RCL 02	
26 PROMPT		76 RCL 13	
27 SF 00		77 *	
28 FS? 22		78 RCL 09	
29 CF 00		79 /	
30 STO 02		80 STO 01	
31 "DP=?"		81 2300	
32 PROMPT		82 X<=Y?	
33 STO 04		83 GTO 02	
34 XEQ 09	-----	84 RDN	
35 FS? 00	1st V	85 /	
36 GTO 03		86 SQRT	
37 RCL 02		87 1/X	
38 X↑2		88 STO 05	
39 *		89 GTO 07	
40 RCL 10		90*LBL 02	
41 *		91 RCL 12	
42 STO 04		92 RCL 05	
43 "DP="		93 -	
44 GTO 10		94 4.67	
45*LBL 03		95 RCL 06	
46 RND		96 *	
47 STO 00		97 RCL 01	
48 XEQ 08		98 /	
49 RND		99 RCL 05	
50 RCL 00	-----	100 *	
	Iterate to find V using 1st V as guess	101 1	
		102 +	
			-----
			Calculate constants
			-----
			Is flow turbulent?
			-----
			Iterate to find $\frac{1}{\sqrt{f}}$

# Program Listings

103 STO 11		155 ARCL 01	
104 LN		156 PROMPT	
105 RCL 07		157 "F="	
106 *		158 RCL 05	
107 -		159 1/X	
108 RCL 11		160 X↑2	
109 1/X		161 ARCL X	
110 CHS		162 PROMPT	
111 1		163 RTN	
112 +		164 .END.	
113 RCL 07		00	
114 *			
115 RCL 05			
116 /			
117 1			
118 +			
119 /			
120 ST+ 05			
121 RCL 05			
122 /			
123 ABS		70	
124 E-3			
125 X<=Y?			
126 GTO 02			
127*LBL 07			
128 RCL 05			
129 1/X			
130 X↑2			
131 RCL 03			
132 *			
133 RCL 13		80	
134 /			
135 RCL 08			
136 +			
137 2			
138 *			
139 RCL 04			
140 RCL 10			
141 /			
142 X<>Y			
143 FS? 00		90	
144 GTO 00			
145 RTN			
146*LBL 00			
147 /			
148 SQRT			
149 STO 02			
150 RTN			
151*LBL 10			
152 ARCL X			
153 PROMPT			
154 "Re="			
	Output	00	



## FLOW WITH A FREE SURFACE

This program solves algebraic manipulations of the following two equations for any of the five variables in each:

Manning flow formula:

$$S = \frac{(nQ)^2}{2.2082 r^{4/3} \times a^2} \quad (1)$$

$$Q = \frac{K}{n} D^{8/3} \times S^{1/2} \quad (2)$$

Where

S = slope of the bottom, dimensionless

n = roughness coefficient

r = hydraulic radius ft.

Q = discharge rate ft<sup>3</sup>/sec

a = crosssection area ft<sup>2</sup>/sec

K = discharge factor dimensionless

and

D = hydraulic diameter

References: Civil Engineering Handbook, Leonard Church Urquhart (ed.), McGraw-Hill Book Company, 4th Ed.  
HP-67/HP-97 Users' Library program #00269D.

- Example: 1. Find Q for  $S = .001$ ,  $N = .013$ ,  $R = 5/12$ , and  $A = 5.0$   
 2. Find K for  $S = .001$ ,  $n = .014$ ,  $Q = 200$ , and  $D = 4$

Solution:

Keystrokes:

[USER]  
 [XEQ] [ALPHA] SIZE [ALPHA] 007  
 [XEQ] [ALPHA] FSFLO [ALPHA]  
 [A]  
 .001 [R/S]  
 .013 [R/S]  
 [R/S]  
 5 [ENT] 12 [÷] [R/S]  
 5 [R/S]  
 [B]  
 .001 [R/S]  
 .014 [R/S]  
 200 [R/S]  
 4 [R/S]  
 [R/S]

Display:

(Set USER mode)

LBL A OR B ?  
 S ?  
 N ?  
 Q ?  
 R ?  
 A ?  
 Q=10.0826  
 S ?  
 N ?  
 Q ?  
 D ?  
 K ?  
 K=2.1962



# Program Listings

01♦LBL "FSF L0" 02 "LBL A 0 R B?" 03 PROMPT 04♦LBL A 05 1.1 06 STO 00 07 CF 22 08 "S ?" 09 XEQ 11 10 "N ?" 11 XEQ 11 12 "Q ?" 13 XEQ 11 14 "R ?" 15 XEQ 11 16 "A ?" 17 XEQ 11 18 RCL 04 19 4 20 ENTER↑ 21 3 22 / 23 Y↑X 24 2.2082 25 * 26 STO 04 27 GTO IND	Equation 1	48 RCL 02 49 RCL 03 50 * 51 X↑2 52 RCL 01 53 / 54 RTN 55♦LBL 15 56 RCL 05 57 X↑2 58 RCL 04 59 * 60 RTN 61♦LBL 02 62 XEQ 15 63 RCL 01 64 * 65 SQRT 66 RCL 03 67 / 68 "N" 69 XEQ 12 70♦LBL 03 71 XEQ 15 72 RCL 01 73 * 74 SQRT 75 RCL 02 76 / 77 "Q" 78 XEQ 12 79♦LBL 05 80 XEQ 16 81 RCL 04 82 / 83 SQRT 84 "A" 85 XEQ 12 86♦LBL 04 87 XEQ 16 88 RCL 05 89 X↑2 90 / 91 2.2082 92 / 93 3 94 ENTER↑ 95 4 96 / 97 Y↑X 98 "R"	Calculate $\frac{(NQ)^2}{S}$
06 28♦LBL 01 29 XEQ 16 30 RCL 01 31 * 32 XEQ 15 33 / 34 "S" 35♦LBL 12 36 "F="	Prompt and store data	55♦LBL 15 56 RCL 05 57 X↑2 58 RCL 04 59 * 60 RTN 61♦LBL 02 62 XEQ 15 63 RCL 01 64 * 65 SQRT 66 RCL 03 67 / 68 "N" 69 XEQ 12 70♦LBL 03 71 XEQ 15 72 RCL 01 73 * 74 SQRT 75 RCL 02 76 / 77 "Q" 78 XEQ 12 79♦LBL 05 80 XEQ 16 81 RCL 04 82 / 83 SQRT 84 "A" 85 XEQ 12 86♦LBL 04 87 XEQ 16 88 RCL 05 89 X↑2 90 / 91 2.2082 92 / 93 3 94 ENTER↑ 95 4 96 / 97 Y↑X 98 "R"	Calculate denominator
37 ARCL X 38 PROMPT 39♦LBL 11 40 PROMPT 41 STO IND	Calculate S	55♦LBL 15 56 RCL 05 57 X↑2 58 RCL 04 59 * 60 RTN 61♦LBL 02 62 XEQ 15 63 RCL 01 64 * 65 SQRT 66 RCL 03 67 / 68 "N" 69 XEQ 12 70♦LBL 03 71 XEQ 15 72 RCL 01 73 * 74 SQRT 75 RCL 02 76 / 77 "Q" 78 XEQ 12 79♦LBL 05 80 XEQ 16 81 RCL 04 82 / 83 SQRT 84 "A" 85 XEQ 12 86♦LBL 04 87 XEQ 16 88 RCL 05 89 X↑2 90 / 91 2.2082 92 / 93 3 94 ENTER↑ 95 4 96 / 97 Y↑X 98 "R"	Calculate N
00 42 RCL 00 43 FC?C 22 44 STO 06 45 ISG 00 46 RTN 47♦LBL 16	Display routine	55♦LBL 15 56 RCL 05 57 X↑2 58 RCL 04 59 * 60 RTN 61♦LBL 02 62 XEQ 15 63 RCL 01 64 * 65 SQRT 66 RCL 03 67 / 68 "N" 69 XEQ 12 70♦LBL 03 71 XEQ 15 72 RCL 01 73 * 74 SQRT 75 RCL 02 76 / 77 "Q" 78 XEQ 12 79♦LBL 05 80 XEQ 16 81 RCL 04 82 / 83 SQRT 84 "A" 85 XEQ 12 86♦LBL 04 87 XEQ 16 88 RCL 05 89 X↑2 90 / 91 2.2082 92 / 93 3 94 ENTER↑ 95 4 96 / 97 Y↑X 98 "R"	Calculate Q
	Input storage routine	55♦LBL 15 56 RCL 05 57 X↑2 58 RCL 04 59 * 60 RTN 61♦LBL 02 62 XEQ 15 63 RCL 01 64 * 65 SQRT 66 RCL 03 67 / 68 "N" 69 XEQ 12 70♦LBL 03 71 XEQ 15 72 RCL 01 73 * 74 SQRT 75 RCL 02 76 / 77 "Q" 78 XEQ 12 79♦LBL 05 80 XEQ 16 81 RCL 04 82 / 83 SQRT 84 "A" 85 XEQ 12 86♦LBL 04 87 XEQ 16 88 RCL 05 89 X↑2 90 / 91 2.2082 92 / 93 3 94 ENTER↑ 95 4 96 / 97 Y↑X 98 "R"	Calculate A
		55♦LBL 15 56 RCL 05 57 X↑2 58 RCL 04 59 * 60 RTN 61♦LBL 02 62 XEQ 15 63 RCL 01 64 * 65 SQRT 66 RCL 03 67 / 68 "N" 69 XEQ 12 70♦LBL 03 71 XEQ 15 72 RCL 01 73 * 74 SQRT 75 RCL 02 76 / 77 "Q" 78 XEQ 12 79♦LBL 05 80 XEQ 16 81 RCL 04 82 / 83 SQRT 84 "A" 85 XEQ 12 86♦LBL 04 87 XEQ 16 88 RCL 05 89 X↑2 90 / 91 2.2082 92 / 93 3 94 ENTER↑ 95 4 96 / 97 Y↑X 98 "R"	Calculate R

# Program Listings

99 XEQ 12		149 RCL 02	
100♦LBL B		150 RCL 03	Calculate K
101 1.1	Equation 2	151 RCL 01	
102 STO 00		152 /	
103 CF 22		153 *	
104 "S ?"		154 RCL 04	
105 XEQ 11	Prompt and store date	155 /	
106 "N ?"		156 "K"	
107 XEQ 11		157 XEQ 12	
108 "Q ?"		158♦LBL 07	
109 XEQ 11		159 RCL 05	Calculate N
110 "D ?"		160 RCL 04	
111 XEQ 11		161 *	
112 "K ?"		162 RCL 03	
113 XEQ 11		163 RCL 01	
114 5	adjust pointer	164 /	
115 ST+ 06		165 /	
116 RCL 01		166 "N"	
117 SQRT		167 XEQ 12	
118 STO 01		168♦LBL 09	
119 RCL 04		169 RCL 03	Calculate D
120 8		170 RCL 01	
121 ENTER↑		171 /	
122 3		172 RCL 02	
123 /		173 *	
124 Y↑X		174 RCL 05	
125 STO 04	$D^{8/3}$	175 /	
126 GTO IND 06		176 3	
127♦LBL 08		177 ENTER↑	
128 RCL 05	Calculate Q	178 8	
129 RCL 02		179 /	
130 /		180 Y↑X	
131 RCL 04		181 "D"	
132 *		182 XEQ 12	
133 RCL 01		183 .END.	
134 *			
135 "Q"			
136 XEQ 12			
137♦LBL 06			
138 RCL 03	Calculate S	90	
139 RCL 05			
140 RCL 02			
141 /			
142 RCL 04			
143 *			
144 /			
145 X↑2			
146 "S"			
147 XEQ 12			
148♦LBL 10		00	



# REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS				
00	Pointer	50	SIZE	007	TOT. REG.	053	USER MODE
	S or NS		ENG		FIX	4	SCI
	n		DEG	x	RAD		GRAD
	Q						ON
	2.2082 r <sup>4/3</sup> or D <sup>8/3</sup>						x OFF
05	a or k	55	FLAGS				
	subroutine pointer		#	INIT S/C	SET INDICATES	CLEAR INDICATES	
10		60					
15		65					
20		70					
25		75					
30		80					
35		85					
			ASSIGNMENTS				
			FUNCTION	KEY	FUNCTION	KEY	
40		90					
45		95					

## PIPE SLIDE-RULE

The program computes the unknown, when given the surface coefficient (n) and any three of the following: 1) Flow (Q); 2) Slope (S); 3) Pipe diameter (D); 4) Depth % (D/d). Also computes Velocity (V). When solving for Pipe diameter, the program automatically rounds up to a standard size of 6", 8", 12", 15", 18", 21", 24", etc.--pipe. Depth percentage (D/d) is found by Newton's method of iteration. In the case of depth percentages between approximately 82% and 100%, two roots or values are appropriate.

Reference: HP-67/97 Users' Library program #00281D by C. B. Coleman.

Example: Find D/d and V given the following:

n = .013	s = .1 (10 ft/100)
Q = 850.3 CFS	D = 144 (inches)

Solution:

Keystrokes:

Display:

[///] [FIX] 2	
[XEQ] [ALPHA] SIZE [ALPHA] 013	
[XEQ] [ALPHA] PSR [ALPHA]	N ?
.013 [R/S]	Q ?
.1 [R/S]	D ?
850.3 [R/S]	S ?
144 [R/S]	D/d ?
[R/S]	D/d=81.96
[R/S] (second solution)	D/d=100.00
[B]	Q ?
850.3 [R/S]	D ?
144 [R/S]	D/d ?
81.96 [R/S]	V=8.57
etc. (for second solution V=7.52)	



# Program Listings

01*LBL "PSR "		49 ISG 04	
02 SF 21	Initialize	50 CLD	
03 SF 27		51 RTN	
04 RAD		52*LBL 10	Solve for Q
05 STOP		53 SF 05	
06*LBL B	Solve for V	54 XEQ 02	
07 SF 06		55 XEQ 15	
08 10		56 "Q"	Output Q
09 STO 04		57 GTO 14	
10 XEQ 05	Input Routine	58*LBL 09	
11 XEQ 02		59 1	Solve for S
12 ENTER↑		60 STO 09	
13 SIN		61 XEQ 20	
14 -		62 X↑2	
15 1/X		63 "S"	Output S
16 RCL 10	Calculate V	64 GTO 14	
17 *		65*LBL 11	
18 RCL 11		66 1	
19 X↑2		67 STO 11	
20 /		68 XEQ 20	
21 1152		69 .375	
22 *		70 Y↑X	
23 "V"		71 6	
24 GTO 14	Output Routine	72 X<>Y	
25*LBL A		73 X<=Y?	
26 8		74 GTO 04	
27 STO 04		75 8	Solve for D
28 "N"		76 X<>Y	
29 XEQ 00		77 X<=Y?	
30 "S"	Input Knowns	78 GTO 04	Rounding to Standard Size
31 XEQ 00		79 12	
32*LBL 05		80 X<>Y	
33 "Q"		81 X<=Y?	
34 XEQ 00		82 GTO 04	
35 "D"		83 3	
36 XEQ 00		84 /	
37 "D/d"		85 .999	
38 XEQ 00		86 +	
39 FS?C 06		87 INT	
40 RTN		88 3	
41 GTO IND		89 *	
03		90 X<>Y	
42*LBL 00		91*LBL 04	
43 "F ?"		92 X<>Y	
44 PROMPT		93 "D"	Output D
45 STO IND	Common Input Routine	94 GTO 14	
04		95*LBL 02	
46 RCL 04		96 RCL 12	
47 FC?C 22		97 50	
48 STO 03		98 /	Common Routine
		99 1	

# Program Listings

100 -		151 STO 01	
101 CHS		152 -	
102 ACOS		153 RCL 02	
103 ST+ X		154 RCL 00	
104 STO 12		155 STO 02	
105 RTN		156 -	
106*LBL 12		157 /	
107 PI	Solve for D/d	158 *	
108 STO 12		159 CHS	
109 4		160 ST+ 12	
110 STO 01		161 RCL 12	
111 CHS		162 /	
112 STO 02		163 RND	
113*LBL 15	Common	164 X≠0?	
114 RCL 11	Iteration	165 GTO 01	
115 0	Routine	166 7	
116 ENTER↑		167 RCL 12	
117 3		168 X>Y?	
118 /		169 GTO 17	
119 Y↑X		170 2	
120 RCL 09		171 /	
121 SQRT		172 COS	
122 *		173 1	
123 RCL 08		174 -	
124 /		175 2	
125 320		176 /	
126 X↑2		177 CHS	
127 /		178 1 E2	
128 STO 05		179 *	
129*LBL 01		180 STO 06	
130 RCL 12		181 .8196	
131 ENTER↑		182 X<>Y	
132 SIN		183 "D/d"	
133 -		184 X<=Y?	
134 5		185 GTO 14	Output D/d
135 Y↑X		186 FC? 07	
136 RCL 12		187 XEQ 14	
137 X↑2		188 FS?C 07	
138 /		189 GTO 14	
139 3		190 SF 07	
140 1/X		191 RCL 12	
141 Y↑X		192 STO 07	
142 RCL 05		193 PI	
143 *		194 ST+ X	
144 FS?C 05		195 STO 01	
145 RTN		196 CHS	
146 RCL 10		197 STO 02	
147 -		198 6	
148 STO 00		199 STO 12	
149 RCL 01		200 GTO 15	
150 RCL 12		201*LBL 20	

# Program Listings

202 SF 05	Output Routine	51	
203 XEQ 02			
204 XEQ 15			
205 RCL 10			
206 /			
207 1/X			
208 RTN			
209*LBL 14			
210 "F="			
211 ARCL X		60	
212 AVIEW			
213 END			
20		70	
30		80	
40		90	
50		00	



## FORCES AT BENDS AND FITTINGS

When the velocity of a flowing fluid is changed in magnitude or direction, such as at a bend or fitting, a force must act upon the fluid to cause the change. This program considers only the systems where the pipe itself is pressure-tight, but where accelerating forces must be resisted by external means to prevent movement of the piping, increased stress in the pipe walls, or both. The equations are:

$$F_x = \frac{QW}{g} (V_{2x} - V_{1x}), \quad F_y = \frac{QW}{g} (V_{2y} - V_{1y})$$

$$\bar{F} = \vec{F}_x + \vec{F}_y, \quad \bar{R} = -\bar{F}$$

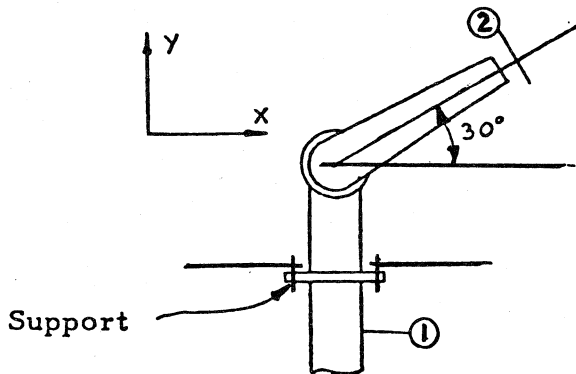
where  $\bar{F}$  = accelerating force on water, lbs  
 $Q$  = rate of flow, ft<sup>3</sup>/sec  
 $W$  = specific weight, lbs/ft<sup>3</sup>  
 $g$  = acceleration of gravity, ft/sec<sup>2</sup>  
 $V_2$  = velocity leaving fittings, ft/sec  
 $V_1$  = velocity entering fitting, ft/sec  
 $\bar{R}$  = reaction of water on fitting, lbs

Subscripts: x for x direction and y for y direction

References: Fluid Mechanics and Hydraulics, by Ronald V. Giles, Schaums Outline Series, McGraw-Hill Book Company, New York, 1962.  
 Hp-67/HP-97 Users' Library program #00268D



Example:



$$Q = 2 \text{ ft.}^3/\text{sec.}$$

$$A_1 = 0.2 \text{ ft.}^2$$

$$A_2 = 0.016 \text{ ft.}^2$$

Find the forces on the water deck gun due to the changes in velocity and direction.

$$V_{,x_1} = 0$$

$$V_{,x_2} = V \cos \theta; \theta = 30^\circ, V = \frac{2}{.016} \left( \frac{Q}{A_2} \right).$$

$$V_{,y_1} = 2/.2 \quad (Q/A_1)$$

$$V_{,y_2} = V \sin \theta; \theta = 30^\circ, V = \frac{2}{.016} \left( \frac{Q}{A_2} \right).$$

Solution:

Keystrokes:

[XEQ] [ALPHA] SIZE [ALPHA] 002

[XEQ] [ALPHA] FORCE [ALPHA]

62.4 [R/S]

2 [R/S]

0 [R/S]

108.25 [R/S]

10 [R/S]

62.5 [R/S]

[R/S]

[R/S]

[R/S]

Display:

W ?

Q ?

V,X1 ?

V,X2 ?

V,Y1 ?

V,Y2 ?

F,X=419.940.0

F,Y=203.6490.0

F=466.7425.9

R=466.74-154.1



# Program Listings

01*LBL "FOR		51	
CE"			
02 "W ?"			
03 PROMPT			
04 "Q ?"			
05 PROMPT			
06 *			
07 32.1739			
08 /	$\frac{WQ}{8}$		
09 STO 00		60	
10 STO 01			
11 "V,X1 ?"			
12 PROMPT			
13 "V,X2 ?"			
14 PROMPT			
15 -			
16 CHS			
17 ST* 00	$F_x$		
18 "V,Y1 ?"			
19 PROMPT		70	
20 "V,Y2 ?"			
21 PROMPT			
22 -			
23 CHS			
24 ST* 01	$F_y$		
25 0			
26 RCL 00			
27 "F,X"			
28 XEQ 08			
29 90		80	
30 RCL 01			
31 "F,Y"			
32 XEQ 08			
33 RCL 00			
34 R-P			
35 "F"			
36 XEQ 08			
37 RCL 01			
38 CHS			
39 RCL 00			
40 CHS		90	
41 R-P			
42 "R"			
43*LBL 08	-----		
44 "I="	Display routine		
45 ARCL X			
46 "I<"			
47 ARCL Y			
48 PROMPT			
49 RTN			
50 .END.		00	

# REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS				
00	QW/g, FX QW/g, FY	50	SIZE	002	TOT. REG.	019	USER MODE
			ENG		FIX	1	SCI
			DEG	x	RAD		GRAD
			ON		OFF	x	
			FLAGS				
			#	INIT S/C	SET INDICATES	CLEAR INDICATES	
05		55					
10		60					
15		65					
20		70					
25		75					
30		80					
35		85					
			ASSIGNMENTS				
			FUNCTION	KEY	FUNCTION	KEY	
40		90					
45		95					

## VALVE SIZING

This program calculates the valve coefficient Cv.

Valve for Liquid flow:

$$Cv = Q \sqrt{\frac{G}{(P1-P2)}}$$

Valve for Gas flow, if  $P2 \geq \frac{P1}{2}$  :

$$Cv = \frac{Q \sqrt{G Ta}}{1360 \sqrt{(P1-P2)P2}}$$

Valve for Gas flow, if  $P2 < \frac{P1}{2}$  :

$$Cv = \frac{Q \sqrt{G Ta}}{1360 (P1/2)}$$

Valve for Vapor flow, if  $P2 \geq \frac{P1}{2}$  :

$$Cv = \frac{Q}{63.4} \sqrt{\frac{Vs}{(P1-P2)}}$$

Valve for Vapor flow, if  $P2 < \frac{P1}{2}$  :

$$Cv = \frac{Q}{63.4} \sqrt{\frac{Vs}{(P1/2)}}$$

Valve for Steam flow, if  $P2 \geq \frac{P1}{2}$  :

$$Cv = \frac{Q (1+0.0007 Ts)}{3 \sqrt{(P1-P2)P2}}$$

Valve for Steam flow, if  $P2 < \frac{P1}{2}$  :

$$Cv = \frac{Q (1+0.0007 Ts)}{3 (P1/2)}$$

References: HP-67/HP-97 Users' Library program #02200D by Paul Crowder.  
 "Process Instruments and Control Handbook" by D. M. Constadine,  
 pub. McGraw-Hill, 1957.

Example: Calculate CV for a gas valve:

Inlet pressure - 135 psig  
 Outlet pressure - 115 psig  
 Sp. Gr. @ flow - 1.0

Flow temp. - 10°F  
 Flow rate - 9000 CFH

Solution:

Keystrokes:

[XEQ] [ALPHA] SIZE [ALPHA] 004

[XEQ] CV

[ALPHA] G [ALPHA] [R/S]

9000 [R/S]

149.7 [R/S]

129.7 [R/S]

1 [R/S]

10 [R/S]

Display:

L,G,V, OR S ?

Q ?

P1 ?

P2 ?

G ?

T ?

CV = 2.82



# Program Listings

01*LBL "CV"		51 XEQ 06	
02 CF 01		52 "VS ?"	
03 "L,G,V, OR S?"		53 PROMPT	
04 PROMPT	Select equation	54 RCL 01	
05 ASTO Y		55 /	
06 "L"		56 SQRT	
07 ASTO X		57 *	
08 X=Y?		58 CF 01	
09 GTO 01		59 XEQ 09	
10 "G"		60*LBL 02	-----
11 ASTO X		61 XEQ 05	Calculate
12 X=Y?		62 RCL 00	CV for gas
13 GTO 02		63 1360	
14 "V"		64 /	
15 ASTO X		65 "G ?"	
16 X=Y?		66 PROMPT	
17 GTO 03		67 "T ?"	
18 XEQ 05		68 PROMPT	
19 "TS ?"	-----	69 460	
20 PROMPT	Calculate	70 +	absolute temp.
21 .0007	CV for steam	71 *	
22 *		72 SQRT	
23 1		73 *	
24 +		74 XEQ 06	
25 3		75 FS?C 01	
26 /		76 GTO 08	
27 RCL 00		77 GTO 10	
28 *		78*LBL 01	-----
29 XEQ 06		79 XEQ 05	Calculate
30 FS?C 01		80 "G ?"	CV for liquid
31 GTO 08		81 PROMPT	
32*LBL 10		82 RCL 01	
33 RCL 01	$P_2 > \frac{P_1}{2}$	83 RCL 02	
34 RCL 02		84 -	
35 *		85 /	
36 SQRT		86 SQRT	
37 /		87 RCL 00	
38 XEQ 09		88 *	
39*LBL 08		89 XEQ 09	
40 RCL 01	$P_2 < \frac{P_1}{2}$	90*LBL 05	-----
41 /		91 "Q ?"	Prompt and
42*LBL 09	-----	92 PROMPT	store input
43 "CV="	Display	93 STO 00	
44 ARCL X	routine	94 "P1 ?"	
45 PROMPT		95 PROMPT	
46*LBL 03		96 STO 01	
47 XEQ 05		97 "P2 ?"	
48 RCL 00	Calculate	98 PROMPT	
49 63.4	CV for vapor	99 STO 02	
50 /		100 RTN	-----
		101*LBL 06	



# Program Listings

102	STO 03	test $\frac{P_1}{2}, P_2$  $P_2 > \frac{P_1}{2}$  $P_2 < \frac{P_1}{2}$	51	
103	RCL 02			
104	RCL 01			
105	2			
106	/			
107	X>Y?			
108	GTO 07			
109	RCL 02			
110	ST- 01			
111	RCL 03			60
112	RTN			
113	LBL 07			
114	STO 01			
115	SF 01			
116	RCL 03			
117	RTN			
118	.END.			
20				70
30			80	
40			90	
50			00	



## PIPE NETWORK ANALYSIS

(Requires at least one additional memory module)

The first portion of the program computes the equivalent length of a pipe by use of the Hazen-Williams equation. This is a prerequisite to any analysis of a water distribution system by the version of the Hardy-Cross Method used herein which requires that all pipes must be of the same diameter  $d$  (normally  $d=10''$  is used) and roughness  $C$  (normally  $C=100$  is used.)

This portion of the program computes the equivalent length by the equation:

$$L_2 = L_1 \left( \frac{C_2}{C_1} \right)^{1.8519} \cdot \left( \frac{d_2}{d_1} \right)^{4.8707}$$

where the subscript 1 represents the existing pipe and the subscript 2 the equivalent pipe.

The second portion of the program computes corrected flows (4 iterations) using the Hardy-Cross method derived here:

Consider a two pipe loop; flow in one pipe  $Q_1$  and the second pipe  $Q_2$ .

- 1) Head Loss (in one pipe) =  $h = KLQ^n$  where  $K$  is a constant dependent on the diameter, roughness and length of the pipe.

$$K = \left( \frac{1.594}{C} \right)^{1.85} \cdot \frac{L}{D^{4.87}}$$

- 2) Balanced head losses ( $H_1$  and  $-H_2$ ) around loop are equal to 0

$$\Sigma H = H_1 - H_2 = 0$$

- 3) If the assumed flow split  $Q_1$  and  $-Q_2$  are each in error by the same amount  $\Delta Q$

$$\Sigma H = \Sigma KL (Q + \Delta Q)^n = 0$$

- 4) Expanding the polynomial and neglecting all but the first two terms

$$\Sigma H = \Sigma KLQ^n + \Sigma nKL\Delta Q \cdot Q^{n-1} = 0 \text{ whence } \Delta Q = \frac{-\Sigma KLQ^n}{n\Sigma KLQ^{n-1}} = \frac{-\Sigma KLQ^n}{n\Sigma KLQ \frac{Q}{Q}}$$

- 5) However, since all pipes are of the same size and roughness,  $K$  cancels. Also  $n = 1.85$  ( $=1/0.54$ )

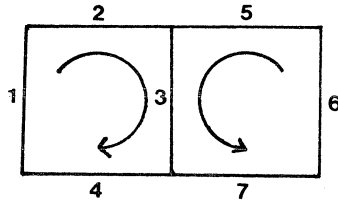
$$\Delta Q = \frac{-\Sigma LQ^{1/0.54}}{\Sigma \left( \frac{LQ^{1/0.54}}{Q(0.54)} \right)}$$

The third portion of the program enables the computation of the pressure (in psi) at any pipe junction in the distribution system given the starting pressure at a particular pipe junction (normally a point where flow enters the system from a pump or elevated tank). This portion of the program computes the head loss in feet along a particular pipe by the formula

$$h_f = L \left[ \left( \frac{3.5521Q}{C} \right)^{1.8519} \cdot d^{-4.8704} \right]$$

Notes:

1. All pipes must be assumed to carry some flow, no matter how small. No zero flows.
2. The program assumes loops comprise 4 pipes. If a loop contains 3 pipes, enter a zero for 4th pipe number.
3. Prior to running the program, sketch the pipe network and assign pipe numbers and flow directions (clockwise or counterclockwise). Adjacent loops must have opposite flow directions to keep the flow consistent in common pipes.



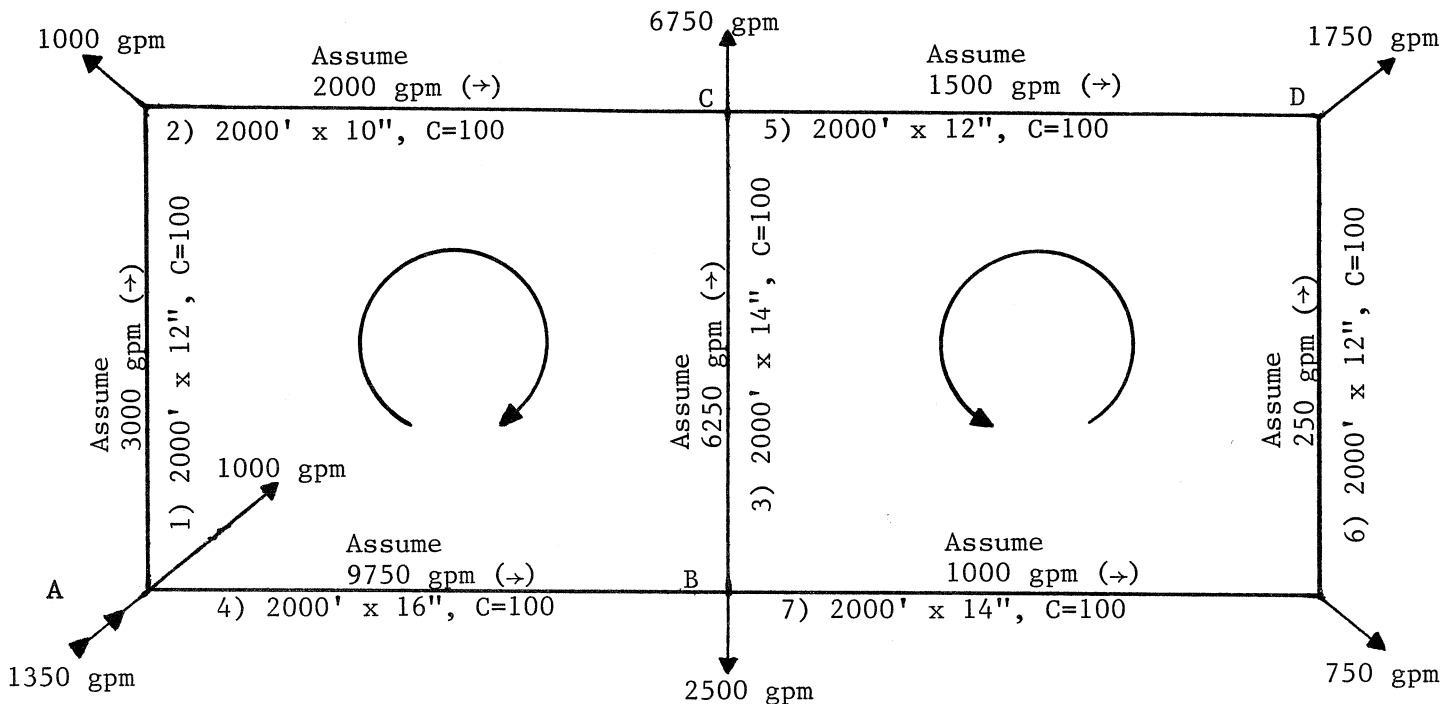
For example, the flow direction in pipe 3 (above) is the same for both loops. Then assign assumed flows in the direction of the arrows positive values and assumed flows opposite the arrows negative values. If the assumed flow in a particular pipe is inadvertently assumed in the wrong direction, the program will automatically correct the sign during the program iterations.

4. SIZE = No. of loops + 2 x No. of pipes + 7.
5. The annunciators in the display show the progress of the calculations (flags 1-4 correspond to iterations 1-4).

Reference: HP-67/HP-97 USERS LIBRARY  
program #02275D by Bernard Golding.

Example:

Compute the correct flows for the network below. Also, find the pressure at point D if the pressure at point A is 100 psi.



Solution:

Keystrokes:

Display:

[USER]

(Set USER mode)

[XEQ] [ALPHA] SIZE [ALPHA] 023

[XEQ] [ALPHA] NA [ALPHA]

PIPE NO. ?

1 [R/S]

PIPE NO. ?

2 [R/S]

PIPE NO. ?

3 [R/S]

PIPE NO. ?

4 [R/S]

A OR B ?

[A]

PIPE NO. ?

3 [R/S]

PIPE NO. ?

5 [R/S]

PIPE NO. ?

6 [R/S]

PIPE NO. ?

7 [R/S]

A OR B ?

[B]	NO. OF PIPES ?
7 [R/S]	EQUIV. DIA. ?
10 [R/S]	EQUIV. RUF. ?
100 [R/S]	L,1 ?
2000 [R/S]	d,1 ?
12 [R/S]	C,1 ?
100 [R/S]	Q,1 ?
3000 [R/S]	L,2 ?
2000 [R/S]	d,2 ?
10 [R/S]	C,2 ?
100 [R/S]	Q,2 ?
2000 [R/S]	L,3 ?
2000 [R/S]	d,3 ?
14 [R/S]	C,3 ?
100 [R/S]	Q,3 ?
6250 [CHS] [R/S]	L,4 ?
2000 [R/S]	d,4 ?
16 [R/S]	C,4 ?
100[R/S]	Q,4 ?
9750 [CHS] [R/S]	L,5 ?
2000 [R/S]	d,5 ?
12 [R/S]	C,5 ?
100 [R/S]	Q,5 ?
1500 [CHS] [R/S]	L,6 ?
2000 [R/S]	d,6 ?
12 [R/S]	C,6 ?
100 [R/S]	Q,6 ?
250 [R/S]	L,7 ?
2000 [R/S]	d,7 ?
14 [R/S]	C,7 ?
100 [R/S]	Q,7 ?
1000 [R/S]	Q,1=3404
[R/S]	Q,2=2404
[R/S]	Q,3=-4134
[R/S]	Q,4=-9346

[R/S]	Q,5=212
[R/S]	Q,6=1962
[R/S]	Q,7=2712
[C]	EQUIV. DIA. ?
10 [R/S]	EQUIV. RUF. ?
100 [R/S]	dP,1=34.55
[R/S]	dP,2=44.09
[R/S]	dP,3=23.37
[R/S]	dP,4=55.24
[R/S]	dP,5=0.20
[R/S]	dP,6=12.45
[R/S]	dP,7=10.71

Since the pressure drops in the direction of the flow (and increases moving upstream), the pressure at point D=100.00 - 55.24 - 23.37 + .20 = 21.59psi.

# User Instructions

				SIZE: 007+
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1	Load the program and set USER mode		[USER]	
2	Initialize the program		[XEQ] NA	PIPE NO. ?
3	Input 4 pipe numbers for each loop.	N	[R/S]	PIPE NO. ?
	Enter a zero for pipe number when there	N	[R/S]	PIPE NO. ?
	are less than 4 pipes in a loop.	N	[R/S]	PIPE NO. ?
		N	[R/S]	A OR B ?
4	For another pipe loop, press		[A]	PIPE NO. ?
	and go to step 3			
5	When all pipe loops are in, press		[B]	NO. OF PIPES ?
6	Input: the number of pipes;	n	[R/S]	EQUIV. DIA. ?
	equivalent diameter;	d	[R/S]	EQUIV. RUF. ?
	and equivalent roughness	C	[R/S]	L,1 ?
7	Input: pipe length;	L,x	[R/S]	d,x ?
	pipe diameter;	d,x	[R/S]	C,x ?
	pipe roughness;	C,x	[R/S]	Q,x ?
	and assumed flow.	$^{+}Q,x$	[R/S]	L,x+1 ?
				or Q,1=C
8	If a mistake is made in putting L,d, or C,			
	press		[GTO] 03	
	and go to step 7		[R/S]	L,x ?
9	Perform step 7 until the data for all pipes			
	is input, at which time the program com-			
	putes corrected flows. If a printer is in			
	the system, the $\Delta Q$ 's will be printed that			
	the user may watch convergence.			
10	To see the corrected flows, press		[R/S]	Q,x=( )
11	Repeat step 9 until x=n.			





# Program Listings

<pre> 01*LBL "NA" 02 FIX 0 03 CF 29 04 CF 01 05 CF 02 06 CF 03 07 CF 04 08 6.1 09 STO 03 </pre>	Initialize	<pre> DIA. "?" 47 PROMPT 48 STO 02 49 "EQUIV. RUF. ?" 50 PROMPT 51 STO 04 52*LBL 03 53 "L," </pre>	
<pre> 10*LBL A 11 ISG 03 12 RCL 03 13 STO 00 14 .01 15 STO 04 16 0 17 STO IND 03 18*LBL 01 19 "PIPE NO . ?" 20 PROMPT 21 RCL 04 22 * 23 ST+ IND 03 24 .01 25 ST* 04 26 RCL 04 27 1 E-9 28 X&lt;=Y? 29 GTO 01 30 "A OR B ?" 31 PROMPT 32*LBL B 33 RCL 03 34 INT 35 STO 03 36 "NO. OF PIPES?" 37 PROMPT 38 STO 06 39 + 40 1 E3 41 / 42 ST+ 03 43 ISG 03 44 1.1 45 STO 01 46 "EQUIV. </pre>	Set up control registers	<pre> 54 XEQ 04 55 RCL 02 56 "d," 57 XEQ 04 58 / 59 2.63 60 ENTER↑ 61 .54 62 / 63 Y↑X 64 * 65 RCL 04 66 "C," 67 XEQ 04 68 / 69 .54 70 1/X 71 Y↑X 72 * 73 STO IND 03 74 RCL 06 75 RCL 03 76 + 77 "Q," 78 XEQ 04 79 STO IND Y 80 ISG 01 81 ISG 03 82 GTO 03 83 .004 84 STO 02 85*LBL 05 86 CF IND 0 2 87 ISG 02 88 GTO 06 89 RCL 00 90 RCL 06 91 + 92 1 </pre>	Compute equivalent lengths, L and store L's and Q's
<pre> 31 PROMPT 32*LBL B 33 RCL 03 34 INT 35 STO 03 36 "NO. OF PIPES?" 37 PROMPT 38 STO 06 39 + 40 1 E3 41 / 42 ST+ 03 43 ISG 03 44 1.1 45 STO 01 46 "EQUIV. </pre>	4th pipe? no	<pre> 87 ISG 02 88 GTO 06 89 RCL 00 90 RCL 06 91 + 92 1 </pre>	iteration counter done, display results
	Prompt and store data		

# Program Listings

93 +		139 SIGN	
94 STO 01		140 *	
95 1		141 RCL IND	
96*LBL 02		Z	
97 "Q,"		142 *	
98 ARCL X		143 ST+ 04	
99 "I="		144 .54	
100 ARCL IND		145 /	
01		146 RCL IND	
101 PROMPT		Y	
102 1		147 /	
103 +		148 ABS	
104 ISG 01		149 ST+ 03	
105 GTO 02		150 GTO 10	
106*LBL 06		151*LBL 04	
107 SF IND 0	set annunciator	152 ARCL 01	input prompting
2		153 "I ?"	
108 RCL 00		154 PROMPT	
109 6		155 RTN	
110 -		156*LBL 09	
111 INT		157 100	extract pipe
112 6		158 ST* 01	numbers
113 +		159 RCL 01	
114 1 E3		160 INT	
115 /		161 ST- 01	
116 7		162 X=0?	done?
117 +		163 RTN	no
118 STO 05		164 RCL 04	
119*LBL 07		165 RCL 03	
120 0		166 /	
121 STO 03	clear E's	167 FS? 55	print ΔQ so user
122 STO 04		168 PRX	can watch con-
123 RCL IND	move control	169 INT	vergence
05	reg. into working	170 STO 03	
124 STO 01	control reg.	171 RCL IND	
125*LBL 10		05	
126 XEQ 09		172 STO 01	adjust Q's by
127 RCL 00	compute ΔQ	173*LBL 11	adding ΔQ
128 +		174 100	
129 ENTER↑		175 ST* 01	
130 ENTER↑		176 RCL 01	
131 RCL 06		177 INT	
132 +		178 ST- 01	done?
133 RCL IND		179 X=0?	yes
X		180 GTO 08	
134 ABS		181 RCL 00	
135 .54		182 RCL 06	
136 1/X		183 +	
137 Y↑X		184 +	
138 RCL IND		185 RCL 03	
Y		186 ST- IND	
		Y	

# Program Listings

187 GTO 11		234 FIX 2	
188♦LBL 08		235 ARCL X	
189 ISG 05		236 PROMPT	
190 GTO 07	do next loop	237 ISG 01	
191 GTO 05	iterate	238 GTO 12	
192♦LBL C	compute pressure	239 .END.	
193 "EQUIV. DIA. ?"	drops		
194 PROMPT	usually 10		
195 STO 02		60	
196 "EQUIV. RUF. ?"			
197 PROMPT	usually 100		
198 STO 04			
199 1.1			
200 STO 01			
201♦LBL 12			
202 RCL 01	pipe no., n		
203 RCL 00			
204 +			
205 ENTER↑		70	
206 ENTER↑			
207 RCL 06			
208 +			
209 RCL IND	$Q_n$		
Y			
210 RCL IND	$L_n$		
Y			
211 ABS			
212 3.5521			
213 *		80	
214 RCL 04			
215 /			
216 .54			
217 1/X			
218 Y↑X			
219 *			
220 RCL 02			
221 2.63			
222 ENTER↑			
223 .54		90	
224 /			
225 CHS			
226 Y↑X			
227 *			
228 .4335			
229 *			
230 "dP, "	$\Delta$ pressure		
231 FIX 0			
232 ARCL 01	display		
233 "f="	result	00	



## RESTRICTION METERING ORIFICE CALCULATIONS

This program solves for orifice bore and for differential pressure across an orifice with flange taps for gas flow.

Equations:

$$C = \frac{Q \text{ NORM}}{7727} \sqrt{\frac{T_F G}{P_F}}$$

$$Y_P = 1 - [0.333 + 1.145 (\beta^2 + 0.7\beta^5 + 12\beta^{13})] \frac{\Delta P}{P_f k}$$

$$S_P = \frac{C}{Y_P \sqrt{h}}, \quad h = 27.7 \Delta P$$

$$S_P = 0.4892\beta^2 + 0.2725\beta^3 - 0.825\beta^4 + 1.75\beta^5$$

$$d = \beta D$$

$$S_f = 0.598\beta^2 + 0.01\beta^3 + 0.00001947\beta^2 (10\beta)^{4.425}$$

$$Y_F = 1 - \left[ \frac{0.41 + 0.35\beta^4}{27.7 P_f k} \right] h_{\text{normF}} \quad h_{\text{normF}} = (C/S_f)^2 / Y_F^2$$

$$h_{\text{max}} = h_{\text{normF}} [Q_{\text{max}} / Q_{\text{normF}}]^2$$

Note: If differential pressure across orifice is too high, the second part of the program will not converge.

- References: L. K. Spink, Principles and Practices of Flow Meter Engineering, 9th Ed., page 167, Plimpton Press, 1967.  
 R. G. Cunningham, Orifice Meters with Supercritical Compressible Flow, pages 625-638, ASTM, July 1951.  
 HP-67/HP-97 Users' Library program #02448D by Larry Richardson.

Example: An orifice is to be sized to control the flow of nitrogen in a 1.939" ID line to 3330 SCFH. A flow transmitter is to be connected to flange taps for an alarm. The temperature is 100°F (560°R), pressure upstream is 8.3 psig (23 psia) pressure downstream is 4.69 psig ( P=3.61 psi). Meter maximum is to be 4500 SCFH.

$$G = \frac{MW_{\text{nitrogen}}}{MW_{\text{air}}} \approx 28/28.95 \approx 0.967$$

$$K_{\text{nitrogen}} = 1.4$$

Solution:

Keystrokes:

[XEQ] [ALPHA] SIZE [ALPHA] 011

[XEQ] [ALPHA] ORF [ALPHA]

3330 [R/S]

560 [R/S]

.967 [R/S]

23 [R/S]

3.61 [R/S]

1.4 [R/S]

1.939 [R/S]

[R/S]

4500 [R/S]

Display:

Q ?

T ?

G ?

P ?

dP ?

K ?

D ?

d=.585 (" bore)

QMAX ?

HM=209. (" water column)





# Program Listings

01♦LBL "ORF		51 RCL 10	
02 "Q ?"		52 X↑2	
03 PROMPT		53 +	
04 "T ?"	Prompt and store	54 1.145	
05 PROMPT	data	55 *	
06 "G ?"		56 .333	
07 PROMPT		57 +	
08 "P ?"		58 RCL 01	
09 PROMPT		59 *	
10 STO 00		60 RCL 00	
11 /		61 /	Y <sub>p</sub>
12 *		62 -	
13 SQRT		63 RCL 09	
14 X<>Y		64 X<>Y	
15 STO 03		65 /	Calculate S <sub>p</sub>
16 *		66 STO 04	
17 STO 09		67 .5	β
18 "dP ?"		68 STO 05	
19 PROMPT		69 STO 06	
20 FIX 3		70♦LBL 01	
21 STO 01		71 RCL 05	
22 27.7		72 RCL 05	
23 *		73 RCL 05	
24 SQRT		74 1.75	
25 ST/ 09		75 *	
26 "K ?"		76 .825	
27 PROMPT		77 -	
28 ST* 00		78 *	
29 "D ?"		79 .2725	
30 PROMPT		80 +	
31 STO 02		81 *	
32 X↑2		82 .58925	
33 7727		83 +	
34 *		84 *	
35 ST/ 09		85 *	S <sub>p</sub> = power series
36 .5	guess for	86 RCL 04	
37 STO 10	β	87 -	
38♦LBL 00		88 X=0?	
39 1		89 GTO 03	
40 RCL 10	Calculate d	90 X<0?	iterate
41 13		91 GTO 04	
42 Y↑X		92 RCL 06	
43 12		93 ST- 05	
44 *		94 GTO 05	
45 RCL 10		95♦LBL 04	
46 5		96 RCL 06	
47 Y↑X		97 ST+ 05	
48 .7		98♦LBL 05	
49 *		99 RCL 06	
50 +		100 RCL 02	
		101 *	

# Program Listings

102 RND		153 X↑2	
103 X=0?		154 .598	
104 GTO 03		155 *	
105 2		156 RCL 02	
106 ST/ 06		157 3	
107 GTO 01		158 Y↑X	
108♦LBL 03		159 .01	
109 RCL 10		160 *	
110 RCL 05		161 +	
111 -		162 RCL 02	
112 RCL 02		163 6.425	
113 *		164 Y↑X	
114 RND		165 .51804	
115 X=0?		166 *	
116 GTO 06		167 +	
117 RCL 05		168 RCL 10	$S_f$
118 STO 10		169 X<>Y	
119 GTO 00		170 /	
120♦LBL 06		171 X↑2	
121 RCL 05	$\beta$	172 STO 10	
122 RCL 02	D	173 STO 07	
123 *		174♦LBL 07	
124 "d="	-----	175 RCL 10	
125 ARCL X	Display	176 1	
126 PROMPT	result	177 RCL 01	
127 FIX 0	-----	178 RCL 07	
128 "QMAX ?"	Calculate $h_m$	179 *	
129 PROMPT		180 -	
130 STO 04		181 X↑2	
131 RCL 01		182 /	
132 27.7		183 STO 08	$h_{normF}$
133 *		184 RCL 07	
134 SQRT		185 -	
135 RCL 09		186 RND	
136 *		187 X=0?	
137 STO 10	C	188 GTO 08	
138 RCL 05	$\beta$	189 RCL 08	
139 4		190 STO 07	
140 Y↑X		191 GTO 07	
141 .35		192♦LBL 08	
142 *		193 RCL 04	$Q_{max}$
143 .41		194 RCL 03	
144 +		195 /	
145 RCL 00		196 X↑2	
146 /		197 RCL 08	
147 27.7		198 *	
148 /		199 "HM="	-----
149 STO 01	[ ] $Y_F$	200 ARCL X	Display
150 RCL 05		201 PROMPT	result
151 STO 02		202 .END.	
152 RCL 02	$\beta$		

# REGISTERS, STATUS, FLAGS, ASSIGNMENTS <sup>47</sup>

DATA REGISTERS			STATUS			
00	KP	50	SIZE	_011	TOT. REG. _056	USER MODE
	used		ENG	_____	FIX <u>3</u>	SCI _____
	used		DEG	<u>x</u>	RAD _____	GRAD _____
	QMAX					ON _____ OFF <u>x</u>
	used		<b>FLAGS</b>			
05	Bnew	55	#	INIT S/C	SET INDICATES	CLEAR INDICATES
	Bincrement					
	old h norm					
	new h norm					
	used					
10	used	60				
15		65				
20		70				
25		75				
30		80				
35		85				
			<b>ASSIGNMENTS</b>			
			FUNCTION	KEY	FUNCTION	KEY
40		90				
45		95				

## ENERGY EQUATION FOR STEADY FLOW

Given any eight of the nine terms in the equation below, the program calculates the unknown term.

Energy Equation:

$$\frac{P_1}{W} + Z_1 + \frac{V_1^2}{2g} + H_p = \frac{P_2}{W} + Z_2 + \frac{V_2^2}{2g} + H_T + H_L$$

where

$H$  = total dynamic head, ft.

$H_p$  = head added by pump, ft.

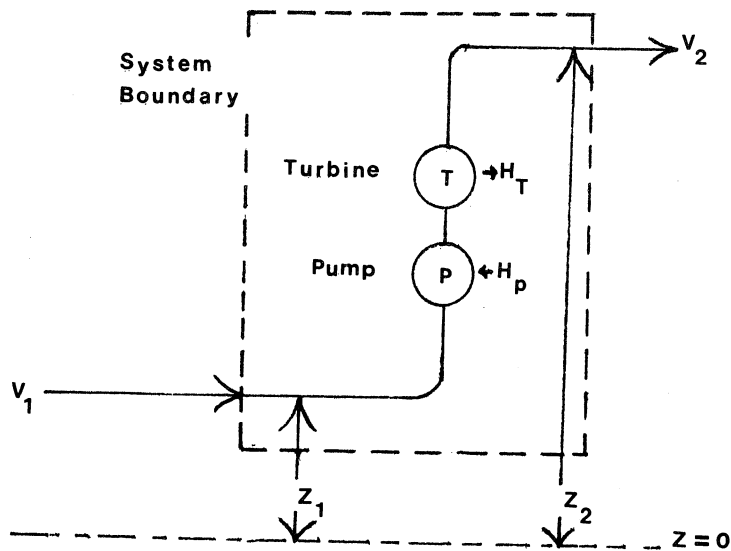
$H_T$  = head extracted by turbine, ft.

$H_L$  = head loss due to friction, ft.

$\frac{V^2}{2g}$  = velocity head, ft.

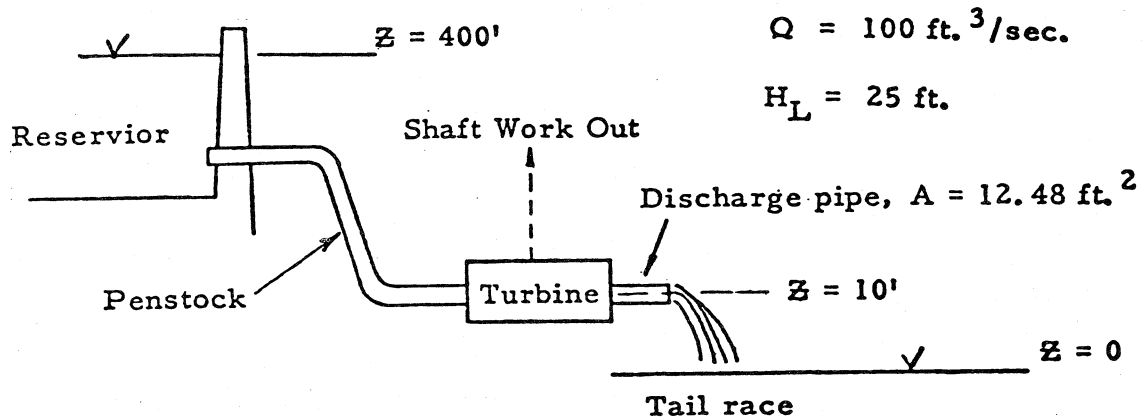
$\frac{P}{W}$  = pressure head, ft.

$Z$  = potential head, ft.



References: HP-67/HP-97 Users' Library program #00267D  
Fluid Mechanics and Hydraulics, by Ronald V. Giles, Schaums  
 Outline Series, McGraw-Hill Book Company, New York, 1962.

Example:



Find the head extracted by the turbine.

Solution:

Keystrokes:

[XEQ] [ALPHA] SIZE [ALPHA] 013  
 [XEQ] [ALPHA] ENRG [ALPHA]  
 0 [R/S]  
 400 [R/S]  
 0 [R/S]  
 0 [R/S]  
 0 [R/S]  
 10 [R/S]  
 100 [ENT] 12.48 [÷] [x<sup>2</sup>] 64.4 [÷] [R/S]  
 [R/S]  
 25 [R/S]

Display:

P1 HEAD ?  
 Z1 HEAD ?  
 V1 HEAD ?  
 HP HEAD ?  
 P2 HEAD ?  
 Z2 HEAD ?  
 V2 HEAD ?  
 HT HEAD ?  
 HL HEAD ?  
 HT HEAD=364.00



# Program Listings

<pre> 01*LBL "ENR G" 02 CF 02 03 SF 01 04 1.1 05 STO 00 06 CF 22 07 "P1" 08 XEQ 15 09 "Z1" 10 XEQ 15 11 "V1" 12 XEQ 15 13 "HP" 14 XEQ 15 15 "P2" 16 XEQ 15 17 "Z2" 18 XEQ 15 19 "V2" 20 XEQ 15 21 "HT" 22 XEQ 15 23 "HL" 24 XEQ 15 25 XEQ 16 26 RCL 11 27 STO 12 28 XEQ 18 29 RCL 12 30 FC? 02 31 X&lt;&gt;Y 32 - 33 CLA 34 ARCL 10 35 "F HEAD= " 36 ARCL X 37 PROMPT 38*LBL 15 39 FS? 01 40 ASTO 10 41 "F HEAD ?" 42 PROMPT 43 STO IND 00 44 FS?C 22 45 GTO 10 46 ST- IND 00 </pre>	<p>Initialize</p>	<pre> 47 CF 01 48 RCL 00 49 5 50 X&lt;=Y? 51 SF 02 52*LBL 10 53 ISG 00 54 RTN 55*LBL 16 56 5.009 57 STO 00 58 0 59*LBL 17 60 RCL IND 00 61 + 62 ISG 00 63 GTO 17 64 STO 11 65 RTN 66*LBL 18 67 1.004 68 STO 00 69 0 70 GTO 17 71 .END. </pre>	<p>RHS or LHS?</p>
	<p>Prompt and store data</p>		<p>Calculate RHS</p>
	<p>Compute unknown</p>	<p>80</p>	<p>Calculate LHS</p>
	<p>Display result</p>		
	<p>Input storage</p>	<p>90</p>	
	<p>Zero results</p>	<p>00</p>	





## COMPRESSIBLE FLOW IN VARIABLE AREA DUCTS

This program solves the area ratio mach number relationship for isentropic flow of a perfect gas in a variable area duct. The program will find M given A/A\* or A/A\* given M, or T/To, P/Po or M given any one of these three quantities. The zero subscript refers to stagnation conditions.

Equations:

$$A/A^* = \frac{1}{M} \left( \frac{1 + \frac{k-1}{2} M^2}{\frac{k+1}{2}} \right)^{\frac{k+1}{2(h-1)}}$$

$$P/P_o = \left( 1 + \frac{k-1}{2} M^2 \right)^{\frac{-k}{h-1}}$$

$$T/T_o = \left( 1 + \frac{k-1}{2} M^2 \right)^{-1}$$

where

T = temperature

P = pressure

A = cross-sectional area of ducts at which M occurs

M = Mach number

A\* = throat area of duct

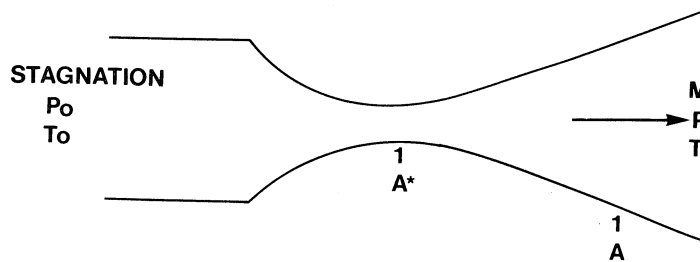
and

$$k = \frac{C_p}{C_n}, \quad C_p = \text{specific heat at constant pressure} \\ C_n = \text{specific heat at constant volume}$$

Notes: The equations apply only to a perfect gas with constant specific heats. An initial guess for M must be supplied for the first equation given above if the area ratio A/A\* is the known quantity. If the guess for M is < 1 then the program converges to a Mach number < 1. If the guess for M is > 1 then the program converges to a solution for M > 1.

References: HP-65 Users' Library program #00780A by Harry Townes.

Example:



For  $K = 1.4$  and  $A/A^* = 1.5$ , find the two possible Mach numbers,  $T/T_0$  and  $P/P_0$ .

Solution:

Keystrokes:

[USER]

[XEQ] [ALPHA] SIZE [ALPHA] 009

[XEQ] [ALPHA] COMFLO [ALPHA]

[A]

1.4 [R/S]

1.5 [R/S]

.5 [R/S]

[A]

1.4 [R/S]

1.5 [R/S]

1.5 [R/S]

[B]

1.4 [R/S]

.4303 [R/S]

[R/S]

[B]

1.4 [R/S]

1.8541 [R/S]

[R/S]

Display:

(Set USER mode)

LBL A OR B ?

K ?

A/A\* ?

GUESS FOR M ?

M=0.4303

K ?

A/A\* ?

GUESS FOR M ?

M=1.8541

K ?

M ?

T/T<sub>0</sub>=0.9643

P/P<sub>0</sub>=0.8805

K ?

M ?

T/T<sub>0</sub>=0.5926

P/P<sub>0</sub>=0.1602



# Program Listings

01*LBL "COM FLO"		49 RCL 05	
02 "LBL A 0 R B ?"		50 -	Calculate M iteratively
03 PROMPT		51 STO 08	
04*LBL A	A/A* vs. M	52 RCL 07	
05 CF 01		53 CHS	
06 "K ?"		54 RCL 01	
07 PROMPT		55 X↑2	
08 1		56 /	
09 +		57 RCL 06	
10 2		58 RCL 02	
11 /		59 1	
12 STO 03		60 -	
13 RCL 03		61 Y↑X	
14 1		62 +	
15 -		63 RCL 08	
16 STO 04		64 X<>Y	
17 /		65 /	
18 2		66 ST- 01	
19 /		67 ABS	
20 STO 02		68 RCL 01	
21 CF 22		69 /	
22 "A/A* ?"		70 1 E-3	
23 PROMPT		71 X<=Y?	
24 FS? 22	Input made?	72 GTO 01	
25 SF 01	yes	73 RCL 01	
26 STO 05		74 GTO 09	
27 "GUESS F OR M?"		75*LBL 02	
28 FC? 22		76 "A/A*"	
29 "M ?"		77 GTO 03	
30 PROMPT		78*LBL B	T/To, P/Po, vs. M
31 STO 01		79 "K ?"	
32*LBL 01		80 PROMPT	
33 RCL 01	Calculate A/A*	81 STO 00	
34 X↑2		82 1	
35 RCL 04		83 -	
36 *		84 ST/ 00	
37 1		85 2	
38 +		86 /	
39 RCL 03		87 STO 02	
40 /		88 CF 22	
41 STO 06		89 "M ?"	
42 RCL 02		90 PROMPT	
43 Y↑X		91 FS? 22	
44 STO 07		92 GTO 04	M input? yes
45 RCL 01		93 "T/To ?"	
46 /		94 PROMPT	
47 FC? 01	A/A*	95 FS? 22	
48 GTO 02		96 GTO 05	
		97 "P/Pa ?"	
		98 PROMPT	
		99 RCL 00	

# Program Listings

100 CHS	Calculate M given P/Po	51		
101 1/X				
102 Y↑X				
103 1				
104 -				
105 RCL 02				
106 /				
107 SQRT				
108♦LBL 09				
109 "M"		60		
110♦LBL 03	----- Display routine			
111 "I="				
112 ARCL X				
113 PROMPT				
114 RTN	----- Calculate T/To			
115♦LBL 04				
116 X↑2				
117 *				
118 1				
119 +		70		
120 STO 01				
121 1/X				
122 "T/To"				
123 XEQ 03		----- Calculate P/Po		
124 RCL 01				
125 RCL 00				
126 Y↑X				
127 1/X				
128 "P/Pa"				
129 XEQ 03				
130♦LBL 05	80			
131 1/X	----- Calculate M given T/To			
132 1				
133 -				
134 RCL 02				
135 /				
136 SQRT				
137 GTO 09				
138 .END.				
40		90		
50		00		

# REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS				
00	K/(K-1) Used (K+1)/2(K-1) or (K-1)/2 (K-1)/2 (K-L)/2	50	SIZE	009	TOT. REG.	052	USER MODE
			ENG		FIX	4	SCI
			DEG	x	RAD		GRAD
							ON
							x
							OFF
05	A/A* Used Used Used	55	FLAGS				
			#	INIT S/C	SET INDICATES	CLEAR INDICATES	
			01	C	calculate M	calculate A/A*	
			22	C	refer to owner's manual		
10		60					
15		65					
20		70					
25		75					
30		80					
35		85					
			ASSIGNMENTS				
			FUNCTION	KEY	FUNCTION	KEY	
40		90					
45		95					

## FLOOD ROUTING AND HYDROGRAPHS

This program calculates either a unit hydrograph or a soil conservation service hydrograph from a given peak time (time of concentration) and peak flow. Any time interval can be selected. The program will also route a given hydrograph through a given dam calculating an outflow hydrograph from given storage conditions and a given outflow structure.

Equations:

### Flood routing

$$I_n + I_{n+1} + \frac{2 S_n}{\Delta t} - O_n = \frac{2 S_{n+1}}{\Delta t} + O_{n+1}$$

where:

I = inflow;

S = storage;

$\Delta t$  = time interval;

O = outflow;

n = cycle number.

### UNIT HYDROGRAPH

$$y = 1.45x^{1.67}, \quad 0.5 > x > 0$$

$$y = 1.16 + \ln x, \quad 0.9 > x > 0.5$$

$$y = \sin(e^{x-1} \cdot 90), \quad 1.2 > x > 0.9$$

$$y = 1.93 - .83 x, \quad 1.6 > x > 1.2$$

$$y = 7.49e^{-1.63x}, \quad x > 1.6$$

SCS HYDROGRAPH

$$y = 1.7 x^2, 0.7 > x > 0$$

$$y = 1.06 + .8 \ln x, 1. > x > 0.7$$

$$y = 1.9 - .83x, 1.8 > x > 1.0$$

$$y = 5.7e^{-1.44x}, x > 1.8$$

where  $x$  = time/time of peak

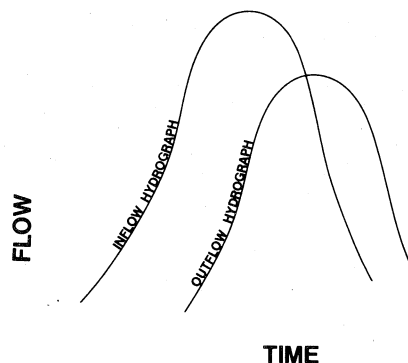
and  $y$  = flow/peak flow

Notes: If a subroutine is used to calculate outflow from  $[\frac{2 S}{\Delta t} + \text{outflow vs. outflow}]$  it must always produce flows greater than or equal to zero.

- References:
1. HP-67/HP-97 USER'S LIBRARY program #01442D by Lawrence Busack
  2. PENNSYLVANIA STATE UNIVERSITY, Hydrologic and Hydraulic Analysis for Small Watersheds, PENN State University, University Park, PA, 1974.
  3. U.S. Department of Interior, Bureau of Reclamation, Design of Small Dams, GPO, Washington, D.C., 1974.
  4. U.S. Department of Agriculture, Soil Conservation Service, National Engineering Handbook Section 4 - Hydrology, GPO, Washington, D.C., 1972.



Example:



A dam with a sharp crested weir spillway is located on a small stream. The spillway is 100 feet wide and has a discharge coefficient of 3.5. At the elevation of the spillway no water is stored. At an elevation of 2 feet above the spillway 100 acre-feet of water is stored and at an elevation of 4 feet above the spillway 250 acre-feet of water is stored. A flood which reaches a peak flow of 1400 cfs in 2.9 hours flows through the dam. Calculate the inflow hydrograph using the SCS curve and the outflow hydrograph. Use a 1/4 hour time interval.

Solution:

First develop the outflow vs.  $\frac{2S}{\Delta t} + \text{outflow}$  relationship

at 2 feet elevation,

$$\begin{aligned} \text{outflow} &= (3.5) (100) (2)^{3/2} [Q=CLH^{3/2}] \\ &= 989.95 \text{ cfs} \\ \frac{2S}{\Delta t} + \text{outflow} &= \left[ \frac{(2) (100) \text{ AC-FT}}{.25 \text{ HRS}} \right] \left[ \frac{43560 \text{ ft}^3}{\text{AC-FT}} \right] \\ &\quad \times \left[ \frac{1}{3600 \frac{\text{SEC}}{\text{HR}}} \right] + 989.95 \\ &= 10669.95 \text{ cfs} \end{aligned}$$

Then, calculating outflow values at each elevation and  $\frac{2S}{\Delta t} + \text{outflow}$  (as above) for 4 feet and interpolating to find intermediate values, the following table is developed:

<u>ELEVATION</u>	<u>OUTFLOW</u>	<u><math>\frac{2S}{\Delta t} + \text{OUTFLOW}</math></u>
0	0	0
1/2	123.74	2543.74
1	350.00	5190.00
1 1/2	642.99	7902.99
2	989.95	10669.95
2 1/2	1383.50	14693.50
3	1818.65	18758.65
3 1/2	2291.77	22861.77
4	2800.00	27000.00

Using a curve-fitting program to yield an analytical expression for the above table,

$$\text{OUTFLOW} \approx 0.11 \left[ \frac{2S}{\Delta t} + \text{outflow} \right] - 200$$

This equation is programmed in subroutine 09.

The hydrographs (inflow and outflow) are then calculated. The keystrokes which follow reflect a printer in the system.

KEYSTROKES:

DISPLAY:

[USER]

(set USER mode)

[XEQ] [ALPHA] SIZE [ALPHA] 009

[XEQ] [ALPHA] HYDRO [ALPHA]

TIME INTVL. ?

.25 [R/S]

TIME, PEAK Q ?

2.90 [R/S]

PEAK Q ?

1400 [R/S]

A,B, OR C ?

[C]

A OR B ?

[B]

T=0.00

IN=0.00

T=0.25

IN=17.69

OUT=0.00

•

•

•

(increment T)

T=1.25

IN=442.18

OUT=0.00

T=1.50

IN=636.74

OUT=86.00

etc.

•

•

•

(increment T)

# User Instructions

				SIZE: 009
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1	Load the program and set USER mode		[USER]	
2	Initialize the program		[XEQ]HYDRO	TIME INTVL. ?
3	Input: time interval;	i	[R/S]	TIME, PEAK Q ?
	time of peak flow;	t peak	[R/S]	PEAK Q ?
	and peak flow.	Q peak	[R/S]	A, B, OR C ?
4	To do flood routing, press		[C]	A OR B ?
5	For a unit hydrograph, press		[A]	T=( )
6	find inflow		[R/S]*	IN=( )
7	flood routing only, find outflow		[R/S]*	OUT=( )
8	Increment T and go to step 6		[R/S]*	T=( )
9	For an SCS hydrograph, press		[B]	T=( )
10	Find inflow		[R/S]*	IN=( )
11	flood routing only, find outflow		[R/S]*	OUT=( )
12	Increment T and go to step 10		[R/S]*	T=( )
	NOTE: If an analytical expression is not known for outflow as a function of $\frac{2S}{\Delta t} +$ outflow, outflow may be read from a graph of the function and input manually at step 7 or 11. To do so, change line 112 from XEQ09 to R/S. When the program stops, enter a value for outflow which corresponds to the value for $\frac{2S}{\Delta t} +$ outflow in the display, and press [R/S] to continue.			
	*These keystrokes are unnecessary if there is a printer in the system.			

# Program Listings

<pre> 01*LBL "HYD R0" 02 CLRG 03 SF 21 04 CF 02 05 "TIME IN TVL. ?" 06 PROMPT 07 STO 01 08 "TIME, P EAK Q?" 09 PROMPT 10 STO 00 11 "PEAK Q ?" 12 PROMPT 13 STO 04 14 "A,B, OR C ?" 15 PROMPT 16*LBL A 17 11 18 STO 08 19 GTO 11 20*LBL B 21 12 22 STO 08 23 GTO 12 24*LBL C 25 SF 02 26 SF 03 27 "A OR B ?" 28 PROMPT 29*LBL 10 30 "T=" 31 ARCL X 32 AVIEW 33 RTN 34*LBL 12 35 RCL 02 36 RCL 00 37 / 38 STO 03 39 .7 40 X&gt;Y? 41 GTO 00 42 X&lt;&gt;Y 43 1 44 X&gt;Y? 45 GTO 01 </pre>	<pre> Initialize ----- Prompt and store data ----- UNIT hydrograph SCS hydrograph do flood routing ----- Display routine ----- SCS hydrograph calculations </pre>	<pre> 46 X&lt;&gt;Y 47 1.8 48 X&gt;Y? 49 GTO 02 50 RCL 03 51 1.44 52 * 53 CHS 54 E↑X 55 5.7 56 * 57 GTO 03 58*LBL 00 59 RCL 03 60 X↑2 61 1.7 62 * 63 GTO 03 64*LBL 01 65 RCL 03 66 LN 67 .8 68 * 69 1.06 70 + 71 1 72 X&gt;Y? 73 X&lt;&gt;Y 74 GTO 03 75*LBL 02 76 RCL 03 77 .83 78 * 79 CHS 80 1.9 81 + 82 1 83 X&gt;Y? 84 X&lt;&gt;Y 85*LBL 03 86 RCL 04 87 * 88 RCL 02 89 "T" 90 XEQ 10 91 RCL 01 92 + 93 STO 02 94 X&lt;&gt;Y 95 "IN" 96 XEQ 10 </pre>	<pre> ----- increment time </pre>
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**NOTES**



**HEWLETT-PACKARD**

**HP-41C**

**USERS' LIBRARY SOLUTIONS**

**Bar Codes**

**Fluid Dynamics and Hydraulics**

FLUID DYNAMICS AND HYDRAULICS

CONDUIT FLOW.....1  
FLOW WITH A FREE SURFACE.....3  
PIPE SLIDE-RULE.....5  
FORCES AT BENDS AND FITTINGS.....7  
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CONDUIT

PROGRAM REGISTERS NEEDED: 38

ROW 1 (1 - 2)



ROW 2 (2 - 8)



ROW 3 (8 - 14)



ROW 4 (15 - 20)



ROW 5 (21 - 24)



ROW 6 (24 - 30)



ROW 7 (31 - 36)



ROW 8 (36 - 44)



ROW 9 (45 - 54)



ROW 10 (54 - 63)



ROW 11 (64 - 69)



ROW 12 (70 - 79)



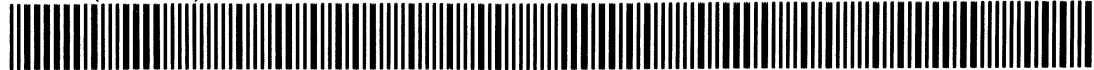
ROW 13 (80 - 88)



ROW 14 (89 - 97)



ROW 15 (98 - 110)



ROW 16 (111 - 122)



ROW 17 (123 - 131)



ROW 18 (132 - 143)



CONDUIT

ROW 19 (144 - 154)



ROW 20 (154 - 161)



ROW 21 (161 - 164)



FLOW WITH A FREE SURFACE

PROGRAM REGISTERS NEEDED: 47

ROW 1 (1 - 2)



ROW 2 (2 - 5)



ROW 3 (5 - 10)



ROW 4 (10 - 14)



ROW 5 (14 - 17)



ROW 6 (18 - 25)



ROW 7 (26 - 33)



ROW 8 (34 - 41)



ROW 9 (42 - 51)



ROW 10 (52 - 62)



ROW 11 (62 - 71)



ROW 12 (71 - 79)



ROW 13 (80 - 87)



ROW 14 (87 - 93)



ROW 15 (94 - 101)



ROW 16 (101 - 106)



ROW 17 (106 - 110)



ROW 18 (110 - 113)



# FLOW WITH A FREE SURFACE

ROW 19 (114 - 125)



ROW 20 (126 - 136)



ROW 21 (136 - 146)



ROW 22 (147 - 156)



ROW 23 (157 - 166)



ROW 24 (167 - 177)



ROW 25 (178 - 183)



PROGRAM REGISTERS NEEDED: 47

ROW 1 (1 : 5)



ROW 2 (6 : 11)



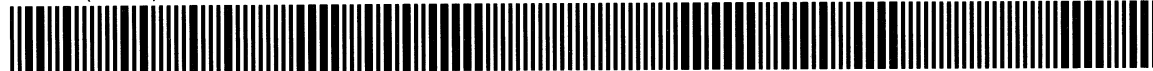
ROW 3 (12 : 21)



ROW 4 (22 : 29)



ROW 5 (29 : 35)



ROW 6 (35 : 39)



ROW 7 (40 : 47)



ROW 8 (47 : 55)



ROW 9 (55 : 62)



ROW 10 (63 : 69)



ROW 11 (69 : 79)



ROW 12 (79 : 87)



ROW 13 (88 : 97)



ROW 14 (98 : 109)



ROW 15 (110 : 121)



ROW 16 (122 : 132)



ROW 17 (133 : 144)



ROW 18 (145 : 157)



ROW 19 (158 : 168)



ROW 20 (169 : 178)



ROW 21 (178 : 183)



ROW 22 (184 : 190)



ROW 23 (190 : 200)



ROW 24 (200 : 206)



ROW 25 (207 : 213)





FORCES AT BENDS AND FITTINGS

PROGRAM REGISTERS NEEDED: 17

ROW 1 (1 - 2)



ROW 2 (3 - 7)



ROW 3 (7 - 13)



ROW 4 (13 - 18)



ROW 5 (18 - 20)



ROW 6 (21 - 28)



ROW 7 (28 - 34)



ROW 8 (35 - 43)



ROW 9 (44 - 50)



ROW 10 (50 - 50)



VALVE SIZING

PROGRAM REGISTERS NEEDED: 32

ROW 1 (1 - 3)



ROW 2 (3 - 6)



ROW 3 (7 - 14)



ROW 4 (14 - 19)



ROW 5 (19 - 27)



ROW 6 (28 - 36)



ROW 7 (37 - 44)



ROW 8 (44 - 51)



ROW 9 (51 - 58)



ROW 10 (58 - 63)



ROW 11 (64 - 69)



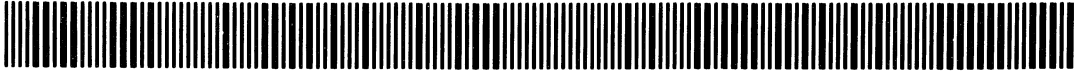
ROW 12 (69 - 77)



ROW 13 (77 - 84)



ROW 14 (85 - 92)



ROW 15 (93 - 97)



ROW 16 (98 - 109)



ROW 17 (110 - 118)



# PIPE NETWORK ANALYSIS

PROGRAM REGISTERS NEEDED: 67

ROW 1 (1 - 5)



ROW 2 (5 - 11)



ROW 3 (12 - 19)



ROW 4 (19 - 23)



ROW 5 (24 - 29)



ROW 6 (30 - 33)



ROW 7 (34 - 36)



ROW 8 (36 - 43)



ROW 9 (43 - 46)



ROW 10 (46 - 49)



ROW 11 (49 - 53)



ROW 12 (53 - 58)



ROW 13 (59 - 66)



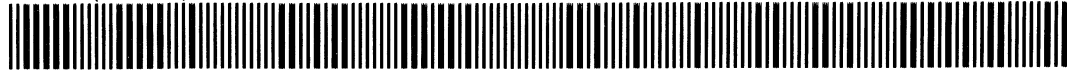
ROW 14 (66 - 73)



ROW 15 (73 - 80)



ROW 16 (80 - 86)



ROW 17 (87 - 97)



ROW 18 (97 - 104)



# PIPE NETWORK ANALYSIS

ROW 19 (104 - 114)



ROW 20 (114 - 124)



ROW 21 (125 - 134)



ROW 22 (135 - 143)



ROW 23 (143 - 150)



ROW 24 (151 - 157)



ROW 25 (158 - 167)



ROW 26 (168 - 175)



ROW 27 (176 - 186)



ROW 28 (186 - 193)



ROW 29 (193 - 193)



ROW 30 (194 - 196)



ROW 31 (196 - 204)



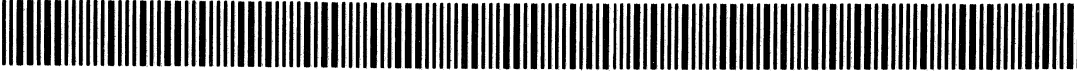
ROW 32 (205 - 212)



ROW 33 (212 - 221)



ROW 34 (221 - 228)



ROW 35 (228 - 233)



ROW 36 (233 - 239)



PIPE NETWORK ANALYSIS

ROW 37 (239 - 239)



RESTRICTION METERING  
ORIFICE CALCULATIONS  
PROGRAM REGISTERS NEEDED: 46

ROW 1 (1 - 4)



ROW 2 (4 - 8)



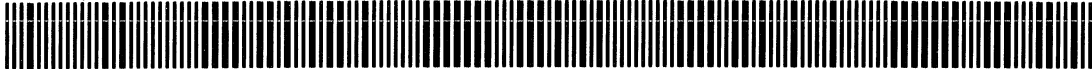
ROW 3 (9 - 18)



ROW 4 (18 - 25)



ROW 5 (26 - 31)



ROW 6 (32 - 39)



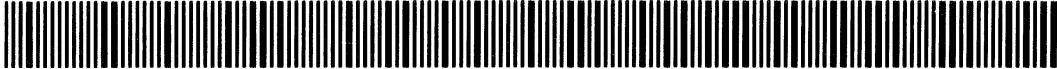
ROW 7 (40 - 49)



ROW 8 (50 - 56)



ROW 9 (56 - 67)



ROW 10 (68 - 76)



ROW 11 (76 - 82)



ROW 12 (82 - 90)



ROW 13 (91 - 99)



ROW 14 (100 - 109)



ROW 15 (110 - 120)



ROW 16 (121 - 128)



ROW 17 (128 - 133)



ROW 18 (134 - 143)



RESTRICTION METERING  
ORIFICE CALCULATIONS

ROW 19 (143 - 152)



ROW 20 (153 - 160)



ROW 21 (161 - 165)



ROW 22 (165 - 177)



ROW 23 (178 - 189)



ROW 24 (190 - 199)



ROW 25 (199 - 202)



ENERGY EQUATION FOR  
STEADY FLOW  
PROGRAM REGISTERS NEEDED: 25

ROW 1 (1 - 4)



ROW 2 (4 - 9)



ROW 3 (9 - 13)



ROW 4 (14 - 18)



ROW 5 (18 - 22)



ROW 6 (22 - 28)



ROW 7 (28 - 35)



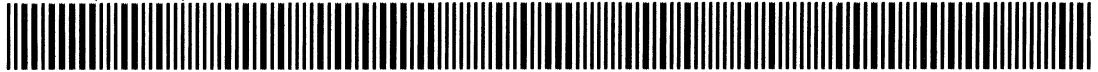
ROW 8 (35 - 40)



ROW 9 (40 - 43)



ROW 10 (44 - 51)



ROW 11 (52 - 58)



ROW 12 (59 - 66)



ROW 13 (66 - 71)



ROW 14 (71 - 71)





COMPRESSIBLE FLOW IN VARIABLE  
AREA DUCTS  
PROGRAM REGISTERS NEEDED: 36

ROW 1 (1 - 2)



ROW 2 (2 - 4)



ROW 3 (5 - 13)



ROW 4 (14 - 22)



ROW 5 (22 - 27)



ROW 6 (27 - 29)



ROW 7 (29 - 40)



ROW 8 (41 - 51)



ROW 9 (52 - 64)



ROW 10 (65 - 72)



ROW 11 (73 - 78)



ROW 12 (79 - 87)



ROW 13 (88 - 93)



ROW 14 (93 - 97)



ROW 15 (97 - 106)



ROW 16 (107 - 115)



ROW 17 (116 - 123)



ROW 18 (123 - 129)



COMPRESSIBLE FLOW IN VARIABLE  
AREA DUCTS

ROW 19 (130 - 138)



# FLOOD ROUTING AND HYDROGRAPHS

PROGRAM REGISTERS NEEDED: 51

ROW 1 (1 - 4)



ROW 2 (4 - 5)



ROW 3 (5 - 8)



ROW 4 (8 - 11)



ROW 5 (11 - 14)



ROW 6 (14 - 20)



ROW 7 (20 - 27)



ROW 8 (27 - 30)



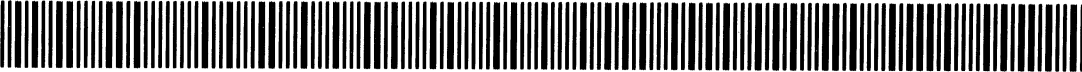
ROW 9 (31 - 41)



ROW 10 (41 - 49)



ROW 11 (50 - 57)



ROW 12 (57 - 66)



ROW 13 (67 - 74)



ROW 14 (75 - 83)



ROW 15 (84 - 93)



ROW 16 (94 - 99)



ROW 17 (100 - 110)



ROW 18 (111 - 118)



# FLOOD ROUTING AND HYDROGRAPHS

ROW 19 (118 - 125)



ROW 20 (126 - 135)



ROW 21 (136 - 142)



ROW 22 (143 - 150)



ROW 23 (150 - 157)



ROW 24 (157 - 163)



ROW 25 (164 - 174)



ROW 26 (175 - 181)



ROW 27 (182 - 189)



ROW 28 (190 - 192)



**NOTES**

**NOTES**

**NOTES**



**HEWLETT  
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Rev. D



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In terms of power and flexibility, the problem-solving potential of the HP-41C programmable calculator is nearly limitless. And in order to see the practical side of this potential, HP has different types of software to help save you time and programming effort. Every one of our software solutions has been carefully selected to effectively increase your problem-solving potential. Chances are, we already have the solutions you're looking for.

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Mechanical Engineering  
Solar Engineering  
Calendars  
Cardiac/Pulmonary  
Chemistry  
Games  
Optometry I (General)  
Optometry II (Contact Lens)  
Physics  
Surveying**

\* Some books require additional memory modules to accommodate all programs.

## **FLUID DYNAMICS AND HYDRAULICS**

CONDUIT FLOW  
FLOW WITH A FREE SURFACE  
PIPE SLIDE-RULE  
FORCES AT BENDS AND FITTINGS  
VALVE SIZING  
PIPE NETWORK ANALYSIS  
RESTRICTION METERING ORIFICE CALCULATIONS  
ENERGY EQUATION FOR STEADY FLOW  
COMPRESSIBLE FLOW IN VARIABLE AREA DUCTS  
FLOOD ROUTING AND HYDROGRAPHS

